## AC/DC Converter

## <High Voltage Safety Precautions>

Read all safety precautions before use

Please note that this document covers only the BM2P151X evaluation board (BM2P151X-EVK-001) and its functions. For additional information, please refer to the datasheet.

## To ensure safe operation, please carefully read all precautions before handling the evaluation board



Depending on the configuration of the board and voltages used,
Potentially lethal voltages may be generated.
Therefore, please make sure to read and observe all safety precautions described in the red box below.

## Before Use

[1] Verify that the parts/components are not damaged or missing (i.e. due to the drops).
[2] Check that there are no conductive foreign objects on the board.
[3] Be careful when performing soldering on the module and/or evaluation board to ensure that solder splash does not occur.
[4] Check that there is no condensation or water droplets on the circuit board.

## During Use

[5] Be careful to not allow conductive objects to come into contact with the board.
[6] Brief accidental contact or even bringing your hand close to the board may result in discharge and lead to severe injury or death.
Therefore, DO NOT touch the board with your bare hands or bring them too close to the board. In addition, as mentioned above please exercise extreme caution when using conductive tools such as tweezers and screwdrivers.
[7] If used under conditions beyond its rated voltage, it may cause defects such as short-circuit or, depending on the circumstances, explosion or other permanent damages.
[8] Be sure to wear insulated gloves when handling is required during operation.

## After Use

[9] The ROHM Evaluation Board contains the circuits which store the high voltage. Since it stores the charges even after the connected power circuits are cut, please discharge the electricity after using it, and please deal with it after confirming such electric discharge.
[10] Protect against electric shocks by wearing insulated gloves when handling.
This evaluation board is intended for use only in research and development facilities and should by handled only by qualified personnel familiar with all safety and operating procedures.
We recommend carrying out operation in a safe environment that includes the use of high voltage signage at all entrances, safety interlocks, and protective glasses.

## AC/DC Converter <br> Non-Isolation Buck Converter PWM method Output 12 W 15 V BM2P151X Reference Board <br> BM2P151X-EVK-001

The BM2P151X-EVK-001 evaluation board outputs 15 V voltage from the input of 90 Vac to 264 Vac . The output current supplies up to 0.8 A . The BM2P151X which is PWM method DC/DC converter IC built-in 650 V MOSFET is used. The BM2P151X contributes to low power consumption by built-in a 650 V starting circuit. Built-in current detection resistor realizes compact power supply design. Current mode control imposes current limitation on every cycle, providing superior performance in bandwidth and transient response. The switching frequency is 65 kHz in fixed mode. At light load, frequency is reduced and high efficiency is realized. Built-in frequency hopping function contributes to low EMI. Low on-resistance $1.5 \Omega 650 \mathrm{~V}$ MOSFET built-in contributes to low power consumption and easy design.


Figure. 1 BM2P151X-EVK-001

## Electronics Characteristics

Not guarantee the characteristics, is representative value.
Unless otherwise noted : $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac}$, lout $=0.5 \mathrm{~A}, \mathrm{Ta}: 25^{\circ} \mathrm{C}$

| Parameter | Min | Typ | Max | Units | Conditions |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | 90 | 230 | 264 | Vac |  |
| Input Frequency | 47 | $50 / 60$ | 63 | Hz |  |
| Output Voltage | 13.5 | 15.0 | 16.5 | V |  |
| Maximum Output Power | - | - | 12.0 | W | lout = 0.8 A |
| Output Current Range ${ }^{\text {(NOTE1) }}$ | 0.0 | 0.5 | 0.8 | A |  |
| Stand-by Power | - | 150 | - | mW | lout = 0 A |
| Efficiency | - | 83.7 | - | $\%$ |  |
| Output Ripple Voltage ${ }^{\text {(NOTE2) }}$ | - | 70 | - | mVpp |  |
| Operating Temperature Range | -10 | +25 | +65 | ${ }^{\circ} \mathrm{C}$ |  |

(NOTE1) Please adjust operating time, within any parts surface temperature under $105{ }^{\circ} \mathrm{C}$
(NOTE2) Not include spike noise

## Operation Procedure

## 1. Operation Equipment

(1) AC Power supply $90 \mathrm{Vac} \sim 264 \mathrm{Vac}$, over 20W
(2) Electronic Load capacity 0.8 A
(3) Multi meter
2. Connect method
(1) AC power supply presetting range 90~264 Vac, Output switch is off.
(2) Load setting under 0.8 A. Load switch is off.
(3) AC power supply $N$ terminal connect to the board $A C(N)$ of CN1, and $L$ terminal connect to $A C(L)$.
(4) Load + terminal connect to VOUT, GND terminal connect to GND terminal
(5) AC power meter connect between AC power supply and board.
(6) Output test equipment connects to output terminal
(7) AC power supply switch ON.
(8) Check that output voltage is 15 V .
(9) Electronic load switch ON
(10) Check output voltage drop by load connect wire resistance


CN1 : from the top (1):AC (L), (2):AC (N)

Figure 2. Connection Circuit

## Deleting

Maximum Output Power Po of this reference board is 12.0 W . The derating curve is shown on the right. If ambient temperature is over $40^{\circ} \mathrm{C}$, Please adjust load continuous time by over $105^{\circ} \mathrm{C}$ of any parts surface temperature.


Figure 3. Temperature Deleting curve

## Application Circuit

$\mathrm{V}_{\mathrm{IN}}=90 \sim 264 \mathrm{Vac}, \mathrm{V}_{\text {Out }}=15 \mathrm{~V}$


Figure 4. BM2P151X-EVK-001 Application Circuit

The BM2P151X is non-insulation method without opto-coupler and feeds back the VCC voltage to 15.0 V typ. This VCC voltage is the voltage between the VCC pin and the GND_IC pin.
The output voltage VOUT is defined by the following equation.

VOUT $=V_{C N T}+V_{F D 2}-V_{F D 1}$
$\mathrm{V}_{\mathrm{CNT}}$ : VCC Control Voltage
$\mathrm{V}_{\mathrm{FD} 1}$ : Forward Voltage of diode D1
$\mathrm{V}_{\mathrm{FD} 2}$ : Forward Voltage of diode D2


Figure 5. General Buck converter application circuit

Compared to the general Buck converter as shown above, the number of parts is reduced because the feedback circuit is not required. However, the output voltage may rise at light load because the VCC voltage and the output voltage that are fed back are different. In that case, please put a resistance on the output terminal and lower the output voltage.

## BM2P151X Overview

## Feature

■ PWM Frequency= 65 kHz

- PWM current mode control

■ Switching frequency jitter

- Burst function around light load
- 650 V Starter

■ 650 V Super-Junction Power MOSFET

- VCC Under voltage detection

■ VCC Over voltage detection

- Cycle by cycle current limiter
- Soft Start function


## Key specifications

■ Operation Voltage Range: VCC: $12.0 \mathrm{~V} \sim 16.97 \mathrm{~V}$ DRAI 650 V (Max)

- Circuit Current(ON):
$0.85 \mathrm{~mA}($ Typ $)$
- Circuit Current (Burst mode):
0.45 mA (Typ)

■ Switching Frequency: 65 kHz (Typ)

- Operating Temperature:
$-40^{\circ} \mathrm{C} \sim+105^{\circ} \mathrm{C}$
■ MOSFET R-ON:
$1.5 \Omega($ Typ $)$


## Dimension

DIP7K


Figure 6. Block Diagram

W (Typ) $\times \mathrm{D}($ Typ $) \times \mathrm{H}($ Max $)$


Figure 7. DIP7K Package

Table 1. BM2P151X PIN description

| No. | Name | I/O |  | ESD Diode |  |
| :---: | :---: | :---: | :--- | :---: | :---: |
|  |  | - | - | - | - |
| 1 | - | - | - | - | - |
| 2 | - | VCC | GND |  |  |
| 3 | GND_IC | I/O | GND | - | - |
| 4 | - | - | - | - | - |
| 5 | VCC | I | Vcc | - | $\checkmark$ |
| 6 | DRAIN | I/O | MOSEFET DRAIN | - | $\checkmark$ |
| 7 | DRAIN | I/O | MOSEFET DRAIN | - | $\checkmark$ |

## Design Overview

1 Important parameter
■ $\quad$ VIN $\quad$ Input Voltage Range AC 90 V ~ $264 \mathrm{Vac}(\mathrm{DC} 100 \mathrm{~V}$ ~ 380 V )

- $V_{\text {OUt }}$ : Output Voltage DC 15 V
- Iout(Typ) : Constant Output Current 0.5 A
- Iout(Max) : Maximum Output Current 0.8 A

■ $\mathrm{f}_{\mathrm{sw}}$ : Switching Frequency Min:60 kHz, Typ: 65 kHz , Max: 70 kHz

- Ipeak(Min) : Over Current Detection Current Min:1.8 A, Typ:2.0 A, Max:2.2A

2 Coil Selection
2.1 Determining Coil Inductance

The switching operation mode determines the $L$ value so that it becomes as discontinuous mode (DCM) as possible. In the continuous mode (CCM), reverse current in trr of the diode flows, which leads to an increase in power loss of diode. Furthermore, this reverse current becomes the peak current when the MOSFET is ON, and the power loss of the MOSFET also increases. The constant load current lout (Typ): 0.5 A , the peak current $\mathrm{I}_{\mathrm{L}}$ flowing through the inductor is:

$$
I_{L}=I_{\text {OUT }}(T y p) \times 2=1.0
$$

It tends to be in continuous mode (CCM) when the input voltage drops. IL Calculate with input voltage minimum voltage 100 Vdc with $20 \%$ margin and $\mathrm{V}_{\mathbb{I N}}(\mathrm{Min})=80 \mathrm{Vdc}$.
From the output voltage $\mathrm{V}_{\text {Out }}: 15 \mathrm{~V}$ and the diode $\mathrm{V}_{\mathrm{F}}: 1 \mathrm{~V}$, Calculate the maximum value of Duty: Duty (Max).

$$
\operatorname{Duty}(\max )=\frac{V_{\text {OUT }}+V_{F}}{V_{I N}(\text { Min })}=0.2
$$



Figure 8. Coil current waveform at OCP detection

From the minimum switching frequency $f_{s w}(\mathrm{Min})=60 \mathrm{kHz}$, Calculate on time ton (Max)

$$
\operatorname{ton}(\text { Max })=\frac{\text { Duty }(\text { Max })}{f_{S W}(\text { Min) }}=3.33 \quad[\mu \mathrm{sec}]
$$

Calculate $L$ value to operate in discontinuous mode.

$$
\mathrm{L}<\operatorname{ton}(M a x) \times \frac{V_{I N}(M i n)-V o}{I_{L}}=216.5 \quad[\mu \mathrm{H}]
$$

2.1 Determining Coil Inductance - Continued

Also, calculate $L$ value so that the overcurrent detection becomes maximum load current $l_{\text {Out }}: 800 \mathrm{~mA}$ or more. Overcurrent detection is calculated by the current flowing through the MOSFET when operating in continuous mode at the minimum switching frequency $f_{s w}(\mathrm{Min})=60 \mathrm{kHz}$. When the current flowing through the MOSFET ( $\neq$ the coil current at switching ON) exceeds the minimum value Ipeak (Min): 1.8 A of the overcurrent detection current, the MOSFET is turned OFF. Since a delay of approximately tdly $=0.1 \mu \mathrm{sec}$ occurs, in reality, the peak current exceeds the lpeak value and the peak current becomes lp. The peak current $I p$ is obtained by setting the current slope at switching $O N$ to $\Delta I_{L}$,

$$
\begin{aligned}
& I_{P}=\text { Ipeak }+\Delta I_{L} \times t d l y \\
& I_{P}=I p e a k+\frac{V_{I N}-V o}{L} \times t d l y
\end{aligned}
$$

Calculate the output current lo (LIM) at overcurrent detection by securing a margin of $10 \%$ from the maximum load current of 800 mA , and setting it as 880 mA .

$$
I_{\text {OUT }}(L I M)=I p-\frac{\text { Iripple }}{2}>I_{\text {OUT }}(\text { Max })
$$

Calculate the minimum value of the $L$ value of the coil. From the above formula,

$$
\mathrm{L}>\frac{\left\{V_{\text {IN }}(\text { Min }) \times t d l y \times f_{\text {SW }}(\text { Min })-\left(V_{\text {OUT }}+V_{F}\right)\right\} \times\left(V_{\text {IN }}(\text { Min })-V_{\text {OUT }}\right)}{2 \times f_{\text {SW }}(\text { Min }) \times\left(I_{\text {OUT }}(\text { Max })-\operatorname{Ipeak}(\text { Min })\right) \times V_{\text {IN }}(\text { Min })}=114.2 \quad[\mu \mathrm{H}]
$$

Therefore, the inductance value of the coil is discontinuous mode when the rated current lo (Typ) is 0.5 A , and in order to detect the overcurrent of the maximum load current lo (Max): 0.8 A or more, the condition of $114.2 \mu \mathrm{H}$ to $216.5 \mu \mathrm{H}$, A coil of $150 \mu \mathrm{H}$ is selected.

### 2.2 Inductor Current Calculation

Calculate the maximum peak current of the inductor. The condition where the peak current is maximized is when the input voltage is the maximum voltage VIN (Max): 380 V , the maximum load current lo (Max): 0.8 A , and the switching frequency is 60 kHz at the minimum. The ripple current Iripple of the coil is given by the following formula.

$$
\text { Iripple }=\frac{d i}{d t} \times t_{\text {ON }}=\frac{\left\{V_{I N}(\operatorname{Max})-\left(V_{\text {OUT }}+V_{F}\right)\right\}}{L} \times \frac{\left(V_{\text {OUT }}+V_{F}\right)}{V_{I N}(\operatorname{Max}) \times f_{S W}(\text { Min })}
$$

2.2 Inductor Current Calculation -Continued

When it is applied to the formula of the peak current,

$$
\begin{equation*}
I p=I_{O U T}(\text { Max })+\frac{\text { Iripple }}{2}=I_{O}+\frac{\left\{V_{I N}(\operatorname{Max})-\left(V_{O U T}+V_{F}\right)\right\}\left(V_{O U T}+V_{F}\right)}{2 \times L \times V_{I N}(\operatorname{Max}) \times f_{S W}(\operatorname{Min})}=1.65 \tag{A}
\end{equation*}
$$

Select a coil with an allowable current of 1.65 A or more.

In this EVK, we use inductance value: $150 \mu \mathrm{H}$, rated: 1.9 A product.

Radial inductor (closed magnetic circuit type) Core size DR09 x 11 series
Product: XF1501Y-151
Manufacturer: ALPHA TRANS CO,. LTD
〒541-0059 Senbanishi KID BIdg 7F, 4-4-11, Bakurou-machi, Chuo-ku, Osaka
http://www.alphatrans.jp/

## 3 Diode Selection

3.1 Flywheel Diode: D1

Flywheel diode uses fast diode (fast recovery diode). The reverse voltage of the diode is $\mathrm{V}_{\text {IN }}(\mathrm{Max}): 380 \mathrm{~V}$ when the output voltage at startup is 0 V . Consider the derating and select 600 V diode. The condition where the effective current of the diode is maximized is when the input voltage is the maximum voltage $\mathrm{V}_{\text {IN }}(\mathrm{Max}): 380 \mathrm{~V}$, the maximum load current lo (Max): 0.8 A , and the switching frequency is 60 kHz at the minimum.

$$
\text { Duty }=\frac{V_{\text {OUT }}+V_{F}}{V_{I N}(\text { Max })}=4.21
$$

The average current ID of the diode is calculated from the peak current Ip: 1.65 A by the following formula

$$
I_{D}(r m s)=I p \times \sqrt{\frac{1-D u t y}{3}}=0.93
$$

Select the rated current of 0.93 A or more.
In fact, we used RFN5BM6S of $5 \mathrm{~A} / 600 \mathrm{~V}$ product as a result of mounting the board and considering the parts temperature.
3.2 VCC Rectifier Diode: D1

Rectifier diodes are used for diodes to supply VCC. The reverse voltage applied to the diode is $\mathrm{V}_{\text {IN }}(\mathrm{Max}): 380 \mathrm{~V}$. Consider the derating and select 600 V diode. Since the current flowing to the IC is small enough, we use the $0.2 \mathrm{~A} / 600 \mathrm{~V}$ RRE02VSM6S.

Design Overview - Continued

4 Capacitor Selection
4.1 Input Capacitor: C4

The input capacitor is determined by input voltage VI and output power POUT. As a guide, for an input voltage of 90 to 264 Vac , $2 \times \mathrm{P}_{\text {out }}[\mathrm{W}] \mu \mathrm{F}$. For 176 to 264 Vac , set $\left.1 \times \mathrm{Pout}_{\mathrm{L}} \mathrm{W}\right] \mu \mathrm{F}$. Since the output power Pout $=12 \mathrm{~W}, 33 \mu \mathrm{~F} / 450 \mathrm{~V}$ is selected at 24 $\mu \mathrm{F}$ or more.

### 4.2 VCC Capacitor: C6

The VCC capacitor C6 is required for stable operation of the device and stable feedback of the output voltage. A withstand voltage of 25 V or more is required, and $1.0 \mu \mathrm{~F}$ to $4.7 \mu \mathrm{~F}$ is recommended. $2.2 \mu \mathrm{~F} / 50 \mathrm{~V}$ is selected.
4.3 Output Capacitor: C7, C8

For the output capacitor, select output voltage $\mathrm{V}_{0}$ of 25 V or more in consideration of derating. For C 7 electrolytic capacitors, capacitance, impedance and rated ripple current must be taken into consideration.
The output ripple voltage is a composite waveform generated by electrostatic capacity: Cout, impedance: ESR when the ripple component of inductor current: $\Delta I_{\mathrm{L}}$ flows into the output capacitor and is expressed by the following formula.

$$
\Delta \text { Vripple }=\Delta I_{L} \times\left(\frac{1}{8 \times \operatorname{Cout} \times f_{s w}}\right)+E S R
$$

The inductor ripple current,

$$
\Delta I_{L}=2 \times\left\{I p-I_{\text {OUT }}(\max )\right\}=2 \times(1.65-0.8)=1.70
$$

For this EVK, we use electrostatic capacity: $680 \mu \mathrm{~F}, \mathrm{ESR}: 0.049 \Omega$, and the design value of output ripple voltage is less than 100 mV .

$$
\Delta \text { Vripple }=\Delta I_{L} \times\left\{\left(\frac{1}{8 \times \text { Cout } \times f_{s w}}\right)+E S R\right\}=1.70 \times\left\{\left(\frac{1}{8 \times 680 \mu \times 65 k}\right)+0.049\right\}=88.1 \quad[\mathrm{mV}]
$$

Next, check whether the ripple current of the capacitor satisfies the rated ripple current. Inductor ripple current RMS conversion,

$$
\begin{equation*}
I_{L}[r m s]=\Delta I_{L} \times \sqrt{\frac{1}{3}}=0.98 \tag{A}
\end{equation*}
$$

The ripple current of the capacitor,

$$
\begin{equation*}
I_{C}[r m s]=\sqrt{I_{L}{ }^{2}-I_{O U T}{ }^{2}}=\sqrt{0.98^{2}-0.8^{2}}=0.57 \tag{A}
\end{equation*}
$$

4.3 Output Capacitor C7, C8 - Continued

Select a rated current of 0.57 A or more.
The output capacitor C 7 used a rated ripple current of 1.24 A at $680 \mu \mathrm{~F} / 25 \mathrm{~V}$.
C 8 has added a $0.1 \mu \mathrm{~F}$ ceramic capacitor to reduce switching noise.

5 Resistor Selection
5.1 Discharge Resistor: R1,R2,R3

The resistor is for discharging X - Capacitor (C1). Considering withstand voltage, 3 pcs of chip resistance of ROHM product MCR18 (200 V withstand voltage) are connected in series. $220 \mathrm{k} \Omega$ is used in 3 pcs in series so that it becomes 45 $V$ or less after 1 second after turning off the power supply.
5.2 Bleeder Resister: R4

Because it is indirectly fed back to the output voltage, the output voltage increases at light load. This board uses bleeder resistance for its improvement. Reducing the resistance value improves the rise in the output voltage of the light load, but increases the power loss. $10 \mathrm{k} \Omega / 0.25 \mathrm{~W}$ is used.

6 EMI Filter Selection
As a measure against "Conducted Emission", Input filter is composed of $X$-Capacitor: C 1 and common mode filter LF1.
X-Capacitor uses $0.22 \mu \mathrm{~F} / \mathrm{X} 2$. The common mode filter uses 13 mH (Min)/1 A.
As a measure against "Radiated Emission", Input filter is composed of Y-Capacitor: C2, C3 and a common mode filter LF2.
Y - Capacitor uses 2200 pF / Y1 and connects the midpoint to the output capacitor so that high frequency noise is not propagated from the input. Moreover, the common mode filter uses $60 \mu \mathrm{H}(\mathrm{Min}) / 1 \mathrm{~A}$ with good characteristics of the 100 MHz band. If "Radiated Emission" does not have a problem in the state that it is loaded in the set, C2, C3, LF2 are unnecessary.

## Performance Data

## Constant Load Regulation



Figure 8. Load Regulation (lout vs. Vout)

Table 2. Load Regulation ( $\mathrm{V}_{\mathrm{IN}}=115 \mathrm{Vac}$ )

| lout | Vout | Efficiency |
| :---: | :---: | :---: |
| 200 mA | 14.699 V | $85.34 \%$ |
| 400 mA | 14.663 V | $85.92 \%$ |
| 600 mA | 14.646 V | $86.19 \%$ |
| 800 mA | 14.632 V | $85.55 \%$ |



Figure 10. Load Regulation (lout vs. Ploss)


Figure 9. Load Regulation (lout vs. Efficiency)

Table 3. Load Regulation ( $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac}$ )

| lout | Vout | Efficiency |
| :---: | :---: | :---: |
| 200 mA | 14.674 V | $81.48 \%$ |
| 400 mA | 14.644 V | $83.20 \%$ |
| 600 mA | 14.628 V | $84.07 \%$ |
| 800 mA | 14.619 V | $83.54 \%$ |



Figure 11. Load Regulation (lout vs. Ploss)

## Performance Data -Continued

Table 4. Load Regulation : $\mathrm{V}_{\mathrm{IN}}=90 \mathrm{Vac}$

| $\begin{gathered} \mathrm{V}_{\mathrm{IN}} \\ {[\mathrm{Vac}]} \\ \hline \end{gathered}$ | $\begin{array}{r} \mathrm{P}_{\mathrm{IN}} \\ {[\mathrm{~W}]} \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{V}_{\text {out }} \\ & {[\mathrm{V}]} \\ & \hline \end{aligned}$ | $\begin{array}{r} \mathrm{I}_{\mathrm{out}} \\ {[\mathrm{~mA}]} \\ \hline \end{array}$ | $\begin{aligned} & \text { Pout } \\ & \text { [W] } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { PLoss }^{\text {[ }} \\ & \text { [W] } \\ & \hline \hline \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Efficiency } \\ \text { [\%] } \\ \hline \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | 0.06 | 15.509 | 0 | 0.000 | 0.055 | 0.00 |
| 90 | 0.06 | 15.435 | 1 | 0.015 | 0.047 | 24.90 |
| 90 | 0.08 | 15.351 | 2 | 0.031 | 0.044 | 40.94 |
| 90 | 0.13 | 15.219 | 5 | 0.076 | 0.049 | 60.88 |
| 90 | 0.16 | 15.190 | 7 | 0.106 | 0.057 | 65.23 |
| 90 | 0.22 | 15.161 | 10 | 0.152 | 0.069 | 68.60 |
| 90 | 0.31 | 15.115 | 15 | 0.227 | 0.082 | 73.37 |
| 90 | 0.39 | 15.036 | 20 | 0.301 | 0.091 | 76.71 |
| 90 | 0.56 | 14.948 | 30 | 0.448 | 0.110 | 80.37 |
| 90 | 0.89 | 14.861 | 50 | 0.743 | 0.149 | 83.30 |
| 90 | 1.23 | 14.808 | 70 | 1.037 | 0.190 | 84.48 |
| 90 | 1.73 | 14.757 | 100 | 1.476 | 0.255 | 85.25 |
| 90 | 2.58 | 14.727 | 150 | 2.209 | 0.368 | 85.72 |
| 90 | 3.42 | 14.709 | 200 | 2.942 | 0.480 | 85.97 |
| 90 | 5.11 | 14.688 | 300 | 4.406 | 0.705 | 86.21 |
| 90 | 6.80 | 14.673 | 400 | 5.869 | 0.932 | 86.30 |
| 90 | 8.49 | 14.663 | 500 | 7.332 | 1.160 | 86.34 |
| 90 | 10.18 | 14.654 | 600 | 8.792 | 1.387 | 86.38 |
| 90 | 13.67 | 14.638 | 800 | 11.710 | 1.955 | 85.70 |
| 90 | 17.20 | 14.622 | 1000 | 14.622 | 2.576 | 85.02 |
| 90 | 20.77 | 14.585 | 1200 | 17.502 | 3.266 | 84.27 |
| 90 | 0.07 | 0.000 | 1210 | 0.000 | 0.070 | 0.00 |
|  |  |  |  |  |  |  |

Table 5. Load Regulation: $\mathrm{V}_{\mathrm{IN}}=100 \mathrm{Vac}$

| $\begin{gathered} \mathbf{V}_{\text {IN }} \\ {[\mathrm{Vac}]} \\ \hline \end{gathered}$ | $\begin{array}{r} \mathrm{P}_{\mathrm{IN}} \\ {[\mathrm{~W}]} \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{V}_{\text {out }} \\ & {[\mathrm{V}]} \\ & \hline \hline \end{aligned}$ | $\begin{gathered} \mathrm{I}_{\text {out }} \\ {[\mathrm{mA}]} \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \text { Pout } \\ & \text { [W] } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline P_{\text {Loss }} \\ & \text { [W] } \\ & \hline \hline \end{aligned}$ | Efficiency [\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 0.06 | 15.528 | 0 | 0.000 | 0.060 | 0.00 |
| 100 | 0.07 | 15.446 | 1 | 0.015 | 0.051 | 23.40 |
| 100 | 0.08 | 15.356 | 2 | 0.031 | 0.048 | 38.88 |
| 100 | 0.13 | 15.208 | 5 | 0.076 | 0.053 | 58.95 |
| 100 | 0.17 | 15.170 | 7 | 0.106 | 0.060 | 63.97 |
| 100 | 0.23 | 15.141 | 10 | 0.151 | 0.074 | 67.29 |
| 100 | 0.32 | 15.116 | 15 | 0.227 | 0.089 | 71.75 |
| 100 | 0.40 | 15.040 | 20 | 0.301 | 0.098 | 75.39 |
| 100 | 0.57 | 14.946 | 30 | 0.448 | 0.118 | 79.22 |
| 100 | 0.90 | 14.856 | 50 | 0.743 | 0.157 | 82.53 |
| 100 | 1.24 | 14.802 | 70 | 1.036 | 0.199 | 83.90 |
| 100 | 1.74 | 14.749 | 100 | 1.475 | 0.264 | 84.81 |
| 100 | 2.59 | 14.718 | 150 | 2.208 | 0.377 | 85.40 |
| 100 | 3.43 | 14.701 | 200 | 2.940 | 0.492 | 85.67 |
| 100 | 5.12 | 14.685 | 300 | 4.406 | 0.718 | 85.99 |
| 100 | 6.81 | 14.669 | 400 | 5.868 | 0.946 | 86.11 |
| 100 | 8.50 | 14.659 | 500 | 7.330 | 1.172 | 86.22 |
| 100 | 10.19 | 14.651 | 600 | 8.791 | 1.395 | 86.30 |
| 100 | 13.67 | 14.638 | 800 | 11.710 | 1.958 | 85.68 |
| 100 | 17.20 | 14.623 | 1000 | 14.623 | 2.581 | 85.00 |
| 100 | 20.81 | 14.603 | 1200 | 17.524 | 3.281 | 84.23 |
| 100 | 20.86 | 14.579 | 1210 | 17.641 | 3.220 | 84.56 |
| 100 | 0.08 | 0.000 | 1220 | 0.000 | 0.083 | 0.00 |

Table 7. Load Regulation: $\mathrm{V}_{\mathrm{IN}}=176 \mathrm{Vac}$

| $\begin{gathered} \mathrm{V}_{\mathrm{IN}} \\ {[\mathrm{Vac}]} \\ \hline \end{gathered}$ | $\begin{array}{r} \mathrm{P}_{\text {IN }} \\ \text { [W] } \\ \hline \end{array}$ | $\begin{aligned} & \mathbf{V}_{\text {OUt }} \\ & {[\mathrm{V}]} \\ & \hline \end{aligned}$ | $\begin{gathered} \mathrm{I}_{\text {OUT }} \\ {[\mathrm{mA}]} \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \text { Pout } \\ & \text { [W] } \\ & \hline \end{aligned}$ | $P_{\text {Loss }}$ [W] | $\begin{array}{\|c\|} \hline \text { Efficiency } \\ {[\%]} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 176 | 0.11 | 15.750 | 0 | 0.000 | 0.105 | 0.00 |
| 176 | 0.11 | 15.626 | 1 | 0.016 | 0.095 | 14.08 |
| 176 | 0.12 | 15.486 | 2 | 0.031 | 0.093 | 24.98 |
| 176 | 0.17 | 15.252 | 5 | 0.076 | 0.098 | 43.83 |
| 176 | 0.21 | 15.181 | 7 | 0.106 | 0.104 | 50.60 |
| 176 | 0.27 | 15.129 | 10 | 0.151 | 0.115 | 56.88 |
| 176 | 0.36 | 15.092 | 15 | 0.226 | 0.138 | 62.19 |
| 176 | 0.46 | 15.075 | 20 | 0.302 | 0.159 | 65.54 |
| 176 | 0.64 | 15.013 | 30 | 0.450 | 0.189 | 70.48 |
| 176 | 0.98 | 14.883 | 50 | 0.744 | 0.231 | 76.32 |
| 176 | 1.31 | 14.819 | 70 | 1.037 | 0.274 | 79.13 |
| 176 | 1.82 | 14.756 | 100 | 1.476 | 0.340 | 81.26 |
| 176 | 2.67 | 14.704 | 150 | 2.206 | 0.459 | 82.76 |
| 176 | 3.52 | 14.688 | 200 | 2.938 | 0.583 | 83.43 |
| 176 | 5.23 | 14.666 | 300 | 4.400 | 0.825 | 84.21 |
| 176 | 6.93 | 14.654 | 400 | 5.862 | 1.064 | 84.63 |
| 176 | 8.62 | 14.645 | 500 | 7.323 | 1.296 | 84.97 |
| 176 | 10.31 | 14.638 | 600 | 8.783 | 1.522 | 85.23 |
| 176 | 13.86 | 14.631 | 800 | 11.705 | 2.154 | 84.46 |
| 176 | 17.51 | 14.618 | 1000 | 14.618 | 2.890 | 83.49 |
| 176 | 21.19 | 14.605 | 1200 | 17.526 | 3.665 | 82.70 |
| 176 | 22.87 | 14.582 | 1290 | 18.811 | 4.056 | 82.26 |
| 176 | 0.17 | 0.000 | 1300 | 0.000 | 0.173 | 0.00 |

## Performance Data -Continued

Table 8. Load Regulation: $\mathrm{V}_{\mathbb{I}}=230 \mathrm{Vac}$

| $\begin{gathered} \mathrm{V}_{\text {IN }} \\ {[\mathrm{Vac}]} \end{gathered}$ | $\begin{gathered} \mathrm{P}_{\mathrm{IN}} \\ {[\mathrm{~W}]} \\ \hline \end{gathered}$ | $\mathrm{V}_{\text {out }}$ [V] | $\begin{gathered} \mathrm{I}_{\text {out }} \\ {[\mathrm{mA}]} \end{gathered}$ | Pout [W] | $\begin{aligned} & P_{\text {Loss }} \\ & \text { [W] } \end{aligned}$ | $\begin{array}{\|c} \hline \text { Efficiency } \\ {[\%]} \\ \hline \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 230 | 0.15 | 15.878 | 0 | 0.000 | 0.151 | 0.00 |
| 230 | 0.16 | 15.744 | 1 | 0.016 | 0.142 | 9.96 |
| 230 | 0.17 | 15.578 | 2 | 0.031 | 0.140 | 18.22 |
| 230 | 0.22 | 15.290 | 5 | 0.076 | 0.145 | 34.59 |
| 230 | 0.26 | 15.201 | 7 | 0.106 | 0.152 | 41.24 |
| 230 | 0.31 | 15.126 | 10 | 0.151 | 0.162 | 48.33 |
| 230 | 0.41 | 15.071 | 15 | 0.226 | 0.182 | 55.41 |
| 230 | 0.51 | 15.045 | 20 | 0.301 | 0.206 | 59.35 |
| 230 | 0.70 | 15.023 | 30 | 0.451 | 0.249 | 64.38 |
| 230 | 1.05 | 14.911 | 50 | 0.746 | 0.303 | 71.07 |
| 230 | 1.39 | 14.831 | 70 | 1.038 | 0.348 | 74.90 |
| 230 | 1.89 | 14.763 | 100 | 1.476 | 0.418 | 77.95 |
| 230 | 2.74 | 14.695 | 150 | 2.204 | 0.537 | 80.42 |
| 230 | 3.60 | 14.674 | 200 | 2.935 | 0.667 | 81.48 |
| 230 | 5.32 | 14.656 | 300 | 4.397 | 0.925 | 82.62 |
| 230 | 7.04 | 14.644 | 400 | 5.858 | 1.182 | 83.20 |
| 230 | 8.74 | 14.635 | 500 | 7.318 | 1.423 | 83.72 |
| 230 | 10.44 | 14.628 | 600 | 8.777 | 1.663 | 84.07 |
| 230 | 14.00 | 14.619 | 800 | 11.695 | 2.305 | 83.54 |
| 230 | 17.80 | 14.610 | 1000 | 14.610 | 3.190 | 82.08 |
| 230 | 21.58 | 14.597 | 1200 | 17.516 | 4.064 | 81.17 |
| 230 | 24.98 | 14.557 | 1370 | 19.943 | 5.037 | 79.84 |
| 230 | 0.25 | 0.000 | 1380 | 0.000 | 0.250 | 0.00 |

Table 9. Load Regulation: $\mathrm{V}_{\mathbb{I}}=264 \mathrm{Vac}$

| $\begin{gathered} \mathrm{V}_{\text {IN }} \\ {[\mathrm{Vac}]} \end{gathered}$ | $\begin{gathered} \mathrm{P}_{\text {IN }} \\ {[\mathrm{W}]} \\ \hline \end{gathered}$ | $\begin{aligned} & \mathbf{V}_{\text {out }} \\ & \text { [V] } \end{aligned}$ | $\begin{gathered} \mathrm{I}_{\text {out }} \\ {[\mathrm{mA}]} \end{gathered}$ | Pout [W] | $P_{\text {Loss }}$ <br> [W] | Efficiency [\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 264 | 0.19 | 15.983 | 0 | 0.000 | 0.187 | 0.00 |
| 264 | 0.19 | 15.830 | 1 | 0.016 | 0.178 | 8.16 |
| 264 | 0.21 | 15.644 | 2 | 0.031 | 0.175 | 15.19 |
| 264 | 0.26 | 15.320 | 5 | 0.077 | 0.180 | 29.81 |
| 264 | 0.30 | 15.220 | 7 | 0.107 | 0.188 | 36.12 |
| 264 | 0.35 | 15.137 | 10 | 0.151 | 0.199 | 43.25 |
| 264 | 0.44 | 15.071 | 15 | 0.226 | 0.218 | 50.92 |
| 264 | 0.54 | 15.038 | 20 | 0.301 | 0.242 | 55.39 |
| 264 | 0.74 | 15.012 | 30 | 0.450 | 0.287 | 61.11 |
| 264 | 1.10 | 14.931 | 50 | 0.747 | 0.356 | 67.68 |
| 264 | 1.44 | 14.845 | 70 | 1.039 | 0.404 | 72.01 |
| 264 | 1.95 | 14.771 | 100 | 1.477 | 0.475 | 75.67 |
| 264 | 2.80 | 14.697 | 150 | 2.205 | 0.594 | 78.76 |
| 264 | 3.66 | 14.669 | 200 | 2.934 | 0.727 | 80.14 |
| 264 | 5.39 | 14.648 | 300 | 4.394 | 0.998 | 81.50 |
| 264 | 7.11 | 14.636 | 400 | 5.854 | 1.259 | 82.31 |
| 264 | 8.83 | 14.627 | 500 | 7.314 | 1.517 | 82.83 |
| 264 | 10.54 | 14.622 | 600 | 8.773 | 1.767 | 83.24 |
| 264 | 14.09 | 14.614 | 800 | 11.691 | 2.399 | 82.98 |
| 264 | 17.93 | 14.595 | 1000 | 14.595 | 3.335 | 81.40 |
| 264 | 21.85 | 14.593 | 1200 | 17.512 | 4.338 | 80.14 |
| 264 | 26.07 | 14.551 | 1410 | 20.517 | 5.553 | 78.70 |
| 264 | 0.31 | 0.000 | 1420 | 0.000 | 0.311 | 0.00 |

## Performance Data -Continued

## Line Regulation



Figure 12. Line Regulation ( $\mathrm{I}_{\mathrm{N}} \mathrm{vs}$. $\mathrm{V}_{\text {OUT }}$ )


Figure 14. Switching Frequency (lout vs. Fsw)


Figure 13. Line Regulation (lin vs. Efficiency)


Figure 15. Coil Peak Current (lout vs. Ipeak)

## Performance Data -Continued

## Operation Waveform



Figure 16. MOSFET $\mathrm{V}_{\mathrm{IN}}=90 \mathrm{Vac}$, Iout $=0.8 \mathrm{~A}$


Figure 18. MOSFET $\mathrm{V}_{\mathrm{IN}}=264 \mathrm{Vac}$, $\mathrm{l}_{\text {out }}=0.8 \mathrm{~A}$


Figure 20. MOSFET VIN $=264$ Vac, Output Short


Figure 17. Diode $\mathrm{V}_{\mathrm{IN}}=90 \mathrm{Vac}$, $\mathrm{I}_{\text {out }}=0.8 \mathrm{~A}$


Figure 19. Diode $\mathrm{V}_{\mathrm{IN}}=264 \mathrm{Vac}$, $\mathrm{I}_{\text {OUT }}=0.8 \mathrm{~A}$


Figure 21. Diode $\mathrm{V}_{\mathbb{I N}}=264 \mathrm{Vac}$, Output Short

## Performance Data -Continued

## Power ON



Figure 22. $\mathrm{V}_{\text {IN }}=115 \mathrm{Vac}$, l $_{\text {OUT }}=0.8 \mathrm{~A}$

Dynamic Response


Figure 24. $\mathrm{V}_{\mathrm{IN}}=115 \mathrm{Vac}$, $\mathrm{l}_{\text {OUT }}=10 \mathrm{~mA} \rightarrow 0.8 \mathrm{~A}$


Figure 26. $\mathrm{V}_{\mathbb{I N}}=230 \mathrm{Vac}$, l $_{\text {OUT }}=10 \mathrm{~mA} \rightarrow 0.8 \mathrm{~A}$


Figure 23. $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac}$, l $_{\text {OUT }}=0.8 \mathrm{~A}$


Figure 25. $\mathrm{V}_{\mathrm{IN}}=115 \mathrm{Vac}$, lout $=0.8 \mathrm{~A} \rightarrow 10 \mathrm{~mA}$


Figure 27. $\mathrm{V}_{\mathrm{IN}_{\mathrm{N}}}=230 \mathrm{Vac}$, $\mathrm{l}_{\text {OUT }}=0.8 \mathrm{~A} \rightarrow 10 \mathrm{~mA}$

## Performance Data -Continued

## Output Ripple Voltage



Figure 28. $\mathrm{V}_{\mathrm{IN}}=115 \mathrm{Vac}, \mathrm{l}_{\text {OUT }}=10 \mathrm{~mA}$


Figure 30. $\mathrm{V}_{\mathbb{I N}}=115 \mathrm{Vac}$, l $_{\text {out }}=0.5 \mathrm{~A}$


Figure 32. $\mathrm{V}_{\mathbb{I N}}=115 \mathrm{Vac}, \mathrm{l}_{\mathrm{OUT}}=0.8 \mathrm{~A}$


Figure 29. $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac}$, $\mathrm{l}_{\text {OUT }}=10 \mathrm{~mA}$


Figure 31. $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac}$, lout $=0.5 \mathrm{~A}$


Figure 33. $\mathrm{V}_{\mathbb{I N}}=230 \mathrm{Vac}, \mathrm{l}_{\text {OUT }}=0.8 \mathrm{~A}$

## Performance Data -Continued

## Parts surface temperature

Table 10. Parts surface temperature
$\mathrm{Ta}=25^{\circ} \mathrm{C}$, measured 30 minites after startup

| Part | Condition |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=90 \mathrm{Vac}, \\ & \text { lout }=0.50 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=90 \mathrm{Vac}, \\ & \text { lout }=0.8 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=264 \mathrm{Vac}, \\ & \text { lout }=0.50 \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} \mathrm{V}_{\text {IN }}=264 \mathrm{Vac}, \\ \text { lout }=0.8 \mathrm{~A} \end{gathered}$ |
| IC1 | $54.4{ }^{\circ} \mathrm{C}$ | $76.5{ }^{\circ} \mathrm{C}$ | $61.5{ }^{\circ} \mathrm{C}$ | $88.7{ }^{\circ} \mathrm{C}$ |
| D1 | $60.3{ }^{\circ} \mathrm{C}$ | $78.6{ }^{\circ} \mathrm{C}$ | $64.3{ }^{\circ} \mathrm{C}$ | $85.8{ }^{\circ} \mathrm{C}$ |
| DB1 | $47.4{ }^{\circ} \mathrm{C}$ | $56.7{ }^{\circ} \mathrm{C}$ | $42.2{ }^{\circ} \mathrm{C}$ | $48.5{ }^{\circ} \mathrm{C}$ |
| L1 | $57.3{ }^{\circ} \mathrm{C}$ | $60.7{ }^{\circ} \mathrm{C}$ | $62.3{ }^{\circ} \mathrm{C}$ | $77.3{ }^{\circ} \mathrm{C}$ |

## EMI

-Conducted Emission: CISPR22 Pub 22 Class B


Figure 34. $\mathrm{V}_{\mathrm{IN}}=110 \mathrm{Vac} / 60 \mathrm{~Hz}$, lout $=0.8 \mathrm{~A}$ $Q P$ margin $=14.0 \mathrm{~dB}, \mathrm{AV}$ margin $=17.1 \mathrm{~dB}$


Figure 35. $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac} / 50 \mathrm{~Hz}$, lout $=0.8 \mathrm{~A}$ QP margin $=10.4 \mathrm{~dB}, \mathrm{AV}$ margin $=7.9 \mathrm{~dB}$
-Radiated Emission: CISPR22 Pub 22 Class B


Figure 36. $\mathrm{V}_{\mathrm{IN}}=110 \mathrm{Vac} / 60 \mathrm{~Hz}$, $\mathrm{I}_{\text {OUt }}=0.8 \mathrm{~A}$
QP margin $=7.3 \mathrm{~dB}$


Figure 37. $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{Vac} / 50 \mathrm{~Hz}$, $\mathrm{l}_{\text {out }}=0.8 \mathrm{~A}$
QP margin $=6.2 \mathrm{~dB}$

Schematics


Figure 38. BM2P151X-EVK-001 Schematics

## Bill of Materials

Table 11. BoM of BM2P151X-EVK-001

| Part <br> Reference | Qty. | Type | Value | Description | Part Number | Manufacture | Configuration mm (inch) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 1 | X2 Capacitor | $0.22 \mu \mathrm{~F}$ | 275Vac, $\pm 20 \%$ | 890324023028CS | Wurth | - |
| C2,C3 | 2 | Y1 Capacitor | 2200pF | Y1 capacitor | DE1E3KX222MB4BP01F | Murata | - |
| C4 | 1 | Electrolytic | $33 \mu \mathrm{~F}$ | 450V, $\pm 20 \%$ | 450BXW33MEFR12.5X20 | Rubycon | $12.5 \mathrm{~mm} \Phi \times 20 \mathrm{~mm}$ |
| C5 | 1 | Ceramic | 100pF | $1 \mathrm{kV}, \mathrm{COG}, \pm 10 \%$ | GRM31A5C3A101J | Murata | 3216 (1206) |
| C6 | 1 | Ceramic | $2.2 \mu \mathrm{~F}$ | 50V, X7R, $\pm 10 \%$ | UMK316B7225KL-T | Taiyo Yuden | 3216 (1206) |
| C7 | 1 | Electrolytic | 680uF | $25 \mathrm{~V}, \pm 20 \%$ | UPA1E681MPD | Nichicon | 10mm@ ${ }^{\text {a }}$ (6mm |
| C8 | 1 | Ceramic | $0.1 \mu \mathrm{~F}$ | 100V, X7R, $\pm 10 \%$ | HMK107B7104MA-T | Taiyo Yuden | 1608 (0603) |
| CN1 | 1 | Connector | 2pin | 5 mm pitch | B2P-NV | JST | - |
| D1 | 1 | FRD | 5A | 600 V | RFN5BM6S | ROHM | TO-252 |
| D2 | 1 | REC Di | 0.2A | 600 V | RRE02VSM6S | ROHM | TUMD2SM |
| DB1 | 1 | Bridge | 1A | 800 V | D1UBA80 | Shindengen | SOP-4 |
| F1 | 1 | Fuse | 1.6A | 1.6A 300V | 36911600000 | Littelfuse | - |
| IC1 | 1 | AC/DC Converter | - | 650V | BM2P151X-Z | ROHM | DIP7 |
| JP1 | 1 | Jumper | - | Jumper Wire | - | - | $\Phi 0.5 \mathrm{~mm}$ |
| L1 | 1 | Coil | $150 \mu \mathrm{H}$ | 1.9A | XF1501Y-151 | Alpha Trans | - |
| LF1 | 1 | Line Filter | 13 mH | 1A | XF1482Y | Alpha Trans | - |
| LF2 | 1 | Line Filter | $60 \mu \mathrm{H}$ | 1A | LF1246Y | Alpha Trans | - |
| PCB | 1 | FR4 | - | - | - | - | - |
| R1,R2,R3 | 3 | Resistor | 220k $\Omega$ | 0.25W, $\pm 5 \%$ | MCR18EZPJ224 | ROHM | 3216 (1206) |
| R4 | 1 | Resistor | $10 \mathrm{k} \Omega$ | 0.25W, $\pm 5 \%$ | MCR18EZPJ103 | ROHM | 3216 (1206) |
| ZNR1 | 1 | Varistor | - | 300Vac, 423Vmin, 400A | V470ZA05P | Littelfuse | $5 \mathrm{~mm} \mathrm{\Phi}$ Disc |

## PCB

## Size : $91 \mathrm{~mm} \times 30 \mathrm{~mm}$



Figure 39. Top Silkscreen (Top view)


Figure 40. Bottom Layout (Top view)

Revision History

| Date | Rev. |  |
| :--- | :--- | :--- |
| Jul.2019 | 001 | New Release |
| Jul.2021 | 002 | - P6 correct L formula and result |

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