

## Input Filter for DCDC Converter

# Design and Application Considerations of Input Filter to reduce Conducted Emissions caused by DC/DC converter

### Introduction

DC/DC converters emit conducted emission noise over power supply lines. Therefore, many DC/DC converter ICs have implemented a spread spectrum feature that lowers noise, with reduced filter component size and BOM cost. However, to really reduce the level of conducted emissions to an acceptable level, an input filter is required. This application note considers both design and application of input filters for DC/DC converters.

### How conducted emissions occur

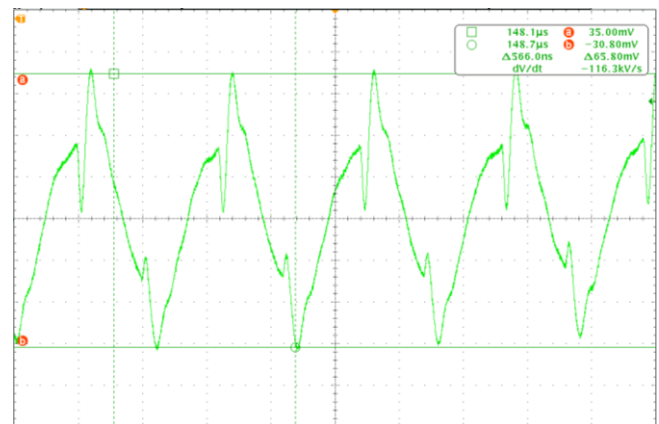
The input current flow of the DC/DC converter alternates with the switching frequency of the DC/DC converter. The input capacitor connected to a converter IC input has an equivalent series resistance (ESR) causing voltage ripples due to the alternating input current flow. The amplitude of this voltage ripple occurring is essentially dependent on the ESR of the used capacitor.

Electrolytic and polymer capacitors have a relatively high ESR. With this kind of capacitors in use, the value of the voltage ripple, which can range from just a few milliohms up to several ohms. Multilayer ceramic capacitors (MLCCs), on the other hand, have a very small ESR of just a few milliohms and thus result in a noise voltage of a few millivolts.

When running an analysis within the time domain, the AC components at the DC/DC converter's input can be analyzed by using an oscilloscope.

This facilitates the measurement of any interference spectrum during the design phase of a DC/DC converter and provides a simple way to estimate any conducted emissions / EMC issues.

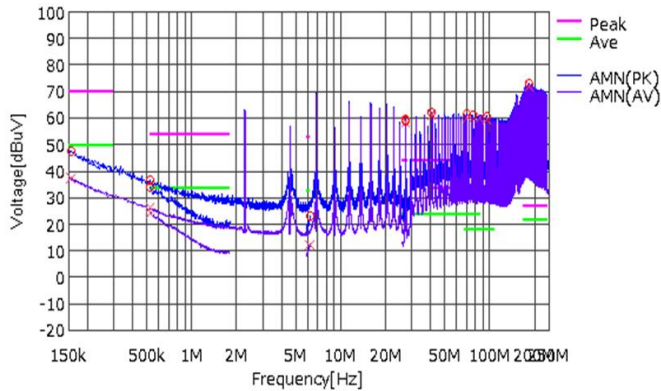
For example, Figure 1 shows the input ripple voltage of an automotive DC/DC converter from the PD9Pxx5EFV-C series.



**FIGURE 1: VOLTAGE RIPPLE AT DC/DC CONVERTER INPUT CAPACITOR**

In this case, the application conditions were 12V DC input voltage, 5V DC output voltage and 1A at resistive load.

MLCCs are state of the art and used in this application example as input capacitors for the DC/DC converter. In this case, despite their low ESR, the input ripple voltage is 68 mV. This ripple voltage leads to differential mode noise and causes conducted emission noise at the DC/DC converter input, as shown in Figure 2.

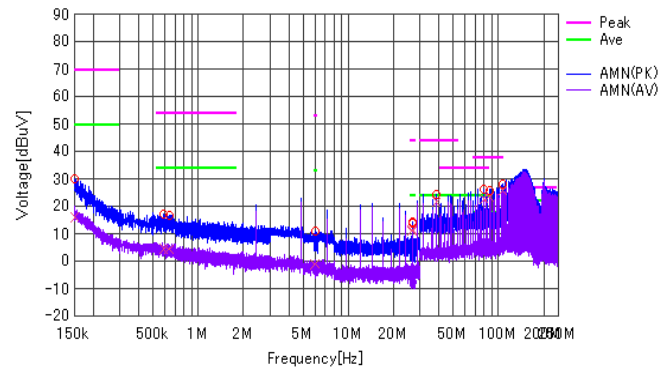


**FIGURE 2: CONDUCTED EMISSION NOISE BY DC/DC CONVERTER WITHOUT INPUT FILTER**

Figure 2 shows conducted emission test results according to the automotive CISPR 25 standard in a frequency range from 150 kHz to 300 MHz. In this case, the spread spectrum has been disabled and the DC/DC converter is in constant PWM mode. The fundamental noise of 2.2 MHz with a highest noise peak of 65 dBμV is equal to the DC/DC converter switching frequency range. Every peak value of further harmonic noise is more than 20 dBμV above the accepted noise limit.

**Reducing conducted emissions**

To reduce conducted emissions caused by a DC/DC converter, an input filter is required in order to pass the electromagnetic compatibility (EMC) test. Figure 3 shows the limited conducted emission results from aforementioned DC/DC converter from the BD9Pxx5EFV-C series.

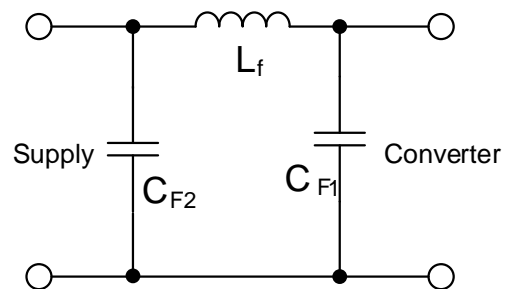


**FIGURE 3: CONDUCTED EMISSION NOISE BY DC/DC CONVERTER WITH INPUT FILTER**

The application conditions were the same as before. Fundamental noise is recognized at the DC/DC converter’s switching frequency in the conducted emission test, as well as further harmonic noise, but the average (AV) and peak (PK) noise levels are reduced over the tested frequency range down to a low, acceptable level.

The main purposes of an input filter are to suppress the noise and surge from the front-stage power supply and to decrease the interference signal at the switching frequency and its harmonic frequencies, to keep them from emitting noise over the power supply and interfering with other devices that use the power supply.

Usually a π-type input filter, as shown in Figure 4, is used for filtering the input current, thereby decreasing the AC amplitude of the voltage ripple, which can reduce the conducted emissions to an acceptable value.



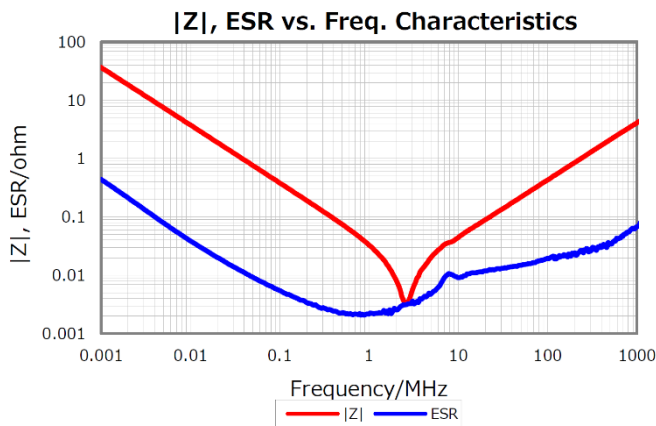
**FIGURE 4: π-TYPE INPUT FILTER**

## Design of input filter

The first step to designing an input filter that will reduce AC amplitude is to place a capacitor at the DC/DC converter IC input. This is also known as a HF bypass capacitor ( $C_{F1}$ ) as shown in Figure 4.

Due to its negligibly low ESR, a ceramic type input capacitor (MLCC) can short-circuit high-frequency voltages to ground with low impedance. The AC ripple has the same frequency as the converter IC switching frequency. The capacitance of the first filter capacitor should be selected with a self-resonance frequency close to the switching frequency.

Figure 5 shows the impedance and ESR curves of a 4.7  $\mu\text{F}$  EIA1206 chip size MLCC capacitor.



**FIGURE 5: CHARACTERISTICS OF 4.7 $\mu\text{F}$  MLCC**

The impedance is lowest at its self-resonant frequency (SRF), where ESR is also low. A low ESR is required so as the peak attenuation characteristic of Z at SRF is not damped. For example, a 4.7  $\mu\text{F}$  EIA0805 chip size MLCC as shown in Figure 5 is the best choice when using a DC/DC converter IC like the BD9Pxx55EFV-C with a switching frequency of 2.2 MHz.

Next, a filter inductor, henceforth referred to as  $L_F$ , and an additional filter capacitor ( $C_{F2}$ ) should be

placed at the input of the DC/DC converter, to form an LC-filter. An LC filter reduces the noise from in- to output by 40 dB / decade.

To reduce noise from a DC/DC converter, the LC filter should be optimized with a corner frequency of 1/10 of the switching frequency. The corner frequency is described in equation (1):

$$(1) \quad f_c = \frac{1}{2\pi \cdot \sqrt{L_f \cdot C_{f2}}}$$

The filter inductor is usually the most expensive part. To reduce BOM costs, an inductor with low inductance can be selected, e.g. 10  $\mu\text{H}$ . To achieve high damping by the filter inductor, it is recommended to select an inductor with an inductance SRF value lower than the capacitance value of the filter capacitor.

The higher the inductance, the smaller the SRF. In practice, a filter inductance with a maximum value of 10  $\mu\text{H}$  is selected since, depending on the design, such an inductance has a self-resonant frequency of approx. 30 MHz.

At low switching frequencies in the range of 60 to 400 KHz, a filter inductor with a metal powder core is suitable. At switching frequencies higher than 1 MHz, ferrite core inductors are preferred.

Exceeding the rated current of the filter inductor may result in damage to the wire winding. Therefore, it is recommended to select an inductor with low DCR so as not to reduce the efficiency of the SMPS.

It is possible to calculate the effective input current of the power module using equation (2):

$$(2) \quad I_{in} = \frac{V_{out} \cdot I_{out}}{V_{in} \cdot \eta}$$

The rated current of the filter coil should be higher than the input current.

The filter capacitor  $C_{F2}$  can be calculated using equation (3).

$$(3) \quad C_{f2} = \frac{1}{(2\pi \cdot 0,1 \cdot f_{sw})^2 \cdot L_f}$$

Depending upon both cost and application, for filter capacitor  $C_{F2}$  an MLCC or electrolytic capacitor can be selected. An electrolytic capacitor has the benefit of a high ESR, which is suitable for damping transient voltages on the power supply line. MLCCs are cheaper than electrolytic capacitors, but have a decreased capacitance as their DC bias voltage is increased.

As an example, figure 6 shows the voltage bias of a 150 nF, 50V, X7R-rated MLCC.

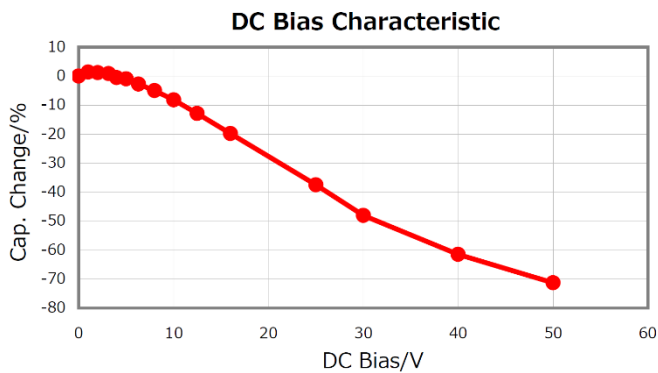


FIGURE 6: OF A 150 NF, 50V RATED X7R MLCC

With respect to the voltage bias of MLCCs, the rated voltage of the MLCC is selected to achieve the required capacitance at an applied voltage. A general guideline is to select a capacitor rating 2 x higher than the highest occurring voltage on the capacitor.

**Filter damping**

The input filter can change or influence the converter transfer function and thus change the loop gain, which is an important measure for the control-loop stability of the DC/DC converter. In other words, adding an input filter can lead to control loop instability if certain conditions are not met.

The input filter has a Q factor (Q) and an output impedance ( $Z_{OutF}$ ), while the DC/DC converter has an input impedance ( $Z_{InCon}$ ), as shown in Figure 7.

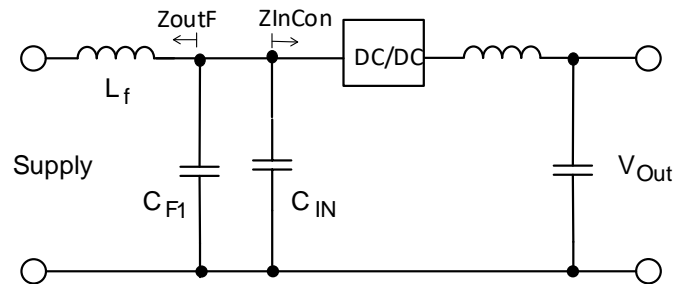


FIGURE 7: IMPEDANCE OF INPUT FILTER AND DCDC CONVERTER

An LC input filter has an effect on the control loop of the DC-DC converter, because the output impedance  $Z_{OutF}$  of the input filter influences the DC/DC converter input  $Z_{InCon}$  impedance. The input filter decreases the phase margin and thus degrades the transient response performance.

When the input filter's Q is too large, oscillations may occur whenever the input voltage changes at the DC/DC converter input, and its control loop can become unstable after applying.

The input filter Q is defined with equation (4):

$$(4) \quad Q = R_d \cdot \sqrt{\frac{C_{F1}}{L_f}}$$

The stability criterion that applies here is that the output impedance of the input filter  $Z_{outF}$  has to be lower than the input impedance of the DC/DC converter input  $Z_{in}$ .

This is described in equation (5):

$$(5) \quad Z_{OutF} \ll Z_{InCon}$$

In addition, the corner frequency  $f_c$  of the input filter should be much lower than the crossover frequency  $f_{COCon}$  of the DC/DC converter.

$$(6) \quad f_c \ll f_{COCon}$$

Adding an R-C network to the filter as shown in Figure 8 lowers the input filter's Q.

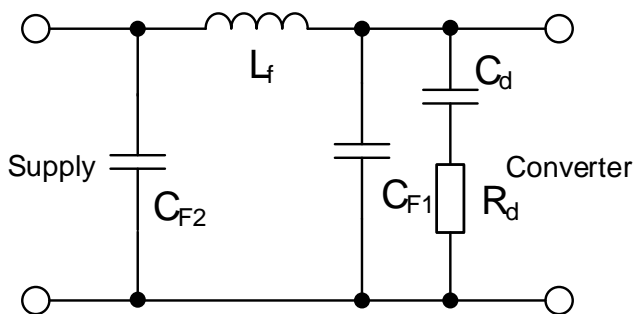


FIGURE 8: INPUT FILTER INCLUDING DAMPING NETWORK

The purpose of the resistor R is to damp the filter, and the purpose of the capacitor in series is to block the DC portion of the input voltage in order to reduce dissipation in the damping resistor.

Equation (7) is used for calculating the damping resistor Rd for a filter with a Q value of  $Q_f = 1$ :

$$(7) \quad R_d = \sqrt{\frac{L_f}{C_{F1}}}$$

A ceramic capacitor  $C_d$  in series with the R-C network has a factor of 5 to 10 of the filter-capacitor capacitance.

$$(8) \quad (5 \cdot C_{F1}) < C_d < (10 \cdot C_{F1})$$

With respect to price and space, alternatively the filter could be damped by selecting an electrolytic capacitor that is connected in parallel to the filter output instead of the R-C network. However, it should be noted that the ESR value of the electrolytic capacitor is not sufficient to have adequate filter attenuation.

## Position of input filter

Optimally, an input filter should be placed as close as possible to the input of the DC/DC converter.

In case the input filter is placed further away due to geometric circumstances, power traces may act as an antenna between the input filter and the DC/DC converter at higher frequencies. These power traces have a capacitive coupling to the housing, causing common mode noise, which leads to radiated emissions.

From another point of view, power trace inductance also acts as a coupling with the ceramic capacitor  $C_{F2}$ , which is shown in Figure 8 as an LC filter. This reduces the voltage ripple to a certain low value, but is not efficient enough to reduce the conducted emissions to a required limit.

## Conclusion

- An input filter is widely used to optimize the EMC of DC/DC SMPS. And in a proper design, the input filter should not cause a stability problem in the DC/DC converter's control loop.
- Adding a  $\pi$ -type input filter limits conducted emission by reducing the DC/DC converter's input voltage ripple.
- The output impedance of the input filter can be matched to the DC/DC converter's input impedance in order to avoid instability.
- The Q factor of the input filter can be reduced with an RC-damping network.

By Stefan Klein, FAE; ATSC

## Reference

- 1) Robert W. Erickson, and Maksimovic Dragan, Fundamentals of Power Electronics, Springer, 25. Mai 2012
- 2) R. D. Middlebrook, Null double injection and the extra element theorem, IEEE Trans. Educ., vol. 32, no. 3, pp. 167–180, Aug. 1998
- 3) Florian Hämmerle, Bode 100 - Application Note, Input Impedance & Filter Stability, OMICRON Lab, 2017
- 4) Capacitor characteristics from Specification of GCM-series, Murata Manufacturing

## Notes

- 1) The information contained herein is subject to change without notice.
- 2) Before you use our Products, please contact our sales representative and verify the latest specifications :
- 3) Although ROHM is continuously working to improve product reliability and quality, semiconductors can break down and malfunction due to various factors.  
Therefore, in order to prevent personal injury or fire arising from failure, please take safety measures such as complying with the derating characteristics, implementing redundant and fire prevention designs, and utilizing backups and fail-safe procedures. ROHM shall have no responsibility for any damages arising out of the use of our Products beyond the rating specified by ROHM.
- 4) Examples of application circuits, circuit constants and any other information contained herein are provided only to illustrate the standard usage and operations of the Products. The peripheral conditions must be taken into account when designing circuits for mass production.
- 5) The technical information specified herein is intended only to show the typical functions of and examples of application circuits for the Products. ROHM does not grant you, explicitly or implicitly, any license to use or exercise intellectual property or other rights held by ROHM or any other parties. ROHM shall have no responsibility whatsoever for any dispute arising out of the use of such technical information.
- 6) The Products specified in this document are not designed to be radiation tolerant.
- 7) For use of our Products in applications requiring a high degree of reliability (as exemplified below), please contact and consult with a ROHM representative : transportation equipment (i.e. cars, ships, trains), primary communication equipment, traffic lights, fire/crime prevention, safety equipment, medical systems, servers, solar cells, and power transmission systems.
- 8) Do not use our Products in applications requiring extremely high reliability, such as aerospace equipment, nuclear power control systems, and submarine repeaters.
- 9) ROHM shall have no responsibility for any damages or injury arising from non-compliance with the recommended usage conditions and specifications contained herein.
- 10) ROHM has used reasonable care to ensure the accuracy of the information contained in this document. However, ROHM does not warrants that such information is error-free, and ROHM shall have no responsibility for any damages arising from any inaccuracy or misprint of such information.
- 11) Please use the Products in accordance with any applicable environmental laws and regulations, such as the RoHS Directive. For more details, including RoHS compatibility, please contact a ROHM sales office. ROHM shall have no responsibility for any damages or losses resulting non-compliance with any applicable laws or regulations.
- 12) When providing our Products and technologies contained in this document to other countries, you must abide by the procedures and provisions stipulated in all applicable export laws and regulations, including without limitation the US Export Administration Regulations and the Foreign Exchange and Foreign Trade Act.
- 13) This document, in part or in whole, may not be reprinted or reproduced without prior consent of ROHM.



Thank you for your accessing to ROHM product informations.  
More detail product informations and catalogs are available, please contact us.

**ROHM Customer Support System**

<http://www.rohm.com/contact/>